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② Optical device comprising a holder accomodating an optical system.

② An optical system is described, for example a radiation source unit (10) supplying a collimated radiation beam (RB), comprising a tubular holder (30) a radiation source (33) arranged in the holder and an optical system having a collimator lens (37). The displacement of the focus of the optical system caused by the variation in length of the holder occurring at a varying temperature can be compensated by a suitable choice of notably the geometry (R, D) and the refractive index (n₁) of the collimator lens.

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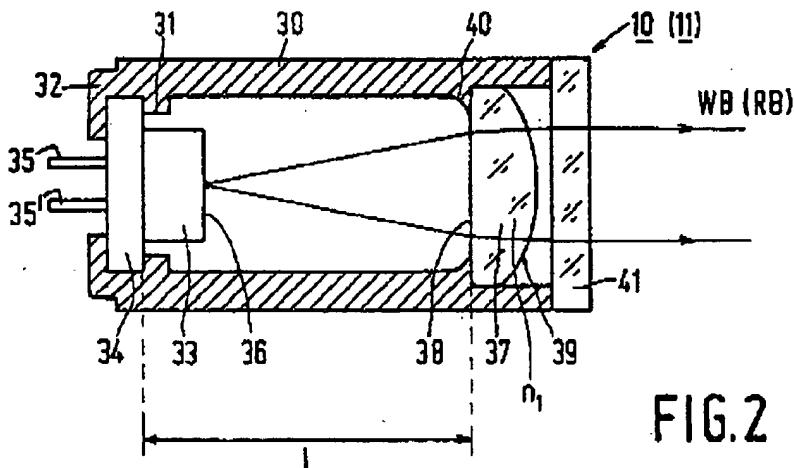


FIG.2

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Optical device comprising a holder accommodating an optical system.

The invention relates to an optical device comprising a holder accommodating a system of optical elements, *inter alia* a lens system, which elements are secured to the inner wall of the holder.

5 A device of this type is known in many embodiments. Examples of such a device is an optical device in the form of a radiation source unit supplying a collimated radiation beam and having a radiation source and a collimator lens whose object focal plane must coincide with the radiating surface of the radiation source. This radiation source unit is used, for example, in an apparatus for scanning an information plane in an optical record carrier with a radiation spot to which apparatus the invention also relates.

10 An apparatus of this type is described in United States Patent no. 4,546,483. An objective system which focuses the parallel beam supplied by the radiation source unit to a scanning spot in the information plane is arranged between the radiation source unit and the record carrier. Scanning an information plane is to be understood to mean both scanning a recorded information plane with a read beam and scanning for the purpose of writing information in this plane with a radiation beam which is intensity-modulated in accordance with the information to be written, as described in United States Patent no. 4,546,483.

15 In order that an optical record carrier can comprise a sufficiently large quantity of information, the optical details of its information structure must have very small dimensions, of the order of one micrometer. The scanning spot must have a corresponding size. Such a scanning spot is obtained with an objective system having a sufficiently large numerical aperture, at least of the order of 0.40, and whose aperture is adequately filled by the beam in such a manner that a diffraction-limited radiation spot is formed in the information plane. It must be ensured that the scanning spot has a constant size and a constant intensity 20 distribution.

25 To this end it is not only required that the focal plane of the objective system always coincides with the information plane, which can be realised in various known manners, but also that the beam entering the objective system and coming from the radiation source unit is always parallel and has a constant cross-section. This means that in the radiation source unit the radiating surface of the radiation source must always coincide with the object focal plane of the collimator lens.

30 The distance between the radiating surface and the collimator lens is determined by the length of the portion of the holder located between these two elements, in which holder the radiation source and the collimator lens are secured. Due to variations of the ambient temperature this length may change so that the radiating surface of the radiation source is moved with respect to the collimator lens. Then the beam supplied by the radiation source unit is no longer optimally parallel. Similar problems may arise in a detection unit for an optical reading and/or recording apparatus, which unit comprises a lens and a radiation detector and for which unit it should be ensured that the spot formed on the detector is not influenced by 35 temperature effects. An analogous problem generally presents itself in optical systems whose elements are secured in a holder having a given coefficient of expansion and in which stringent requirements are imposed on the mutual positioning of the optical elements.

40 The present invention has for its object to provide a general solution to this problem and to provide optical devices whose optical behaviour is substantially independent of temperature variations. An optical device according to the invention is characterized in that the equivalent coefficient of expansion of the optical system giving the change in the optical behaviour of this system as a function of the temperature and being determined by:

- the coefficients of expansion of the materials of the optical elements,
- the refractive indices of these materials and their variations with temperature,
- the dimensions of the optical elements and
- the temperature dependency of the wavelength of the optical beam passing through the device is equal to 45 the coefficient of expansion of the holder material which is located between the fixations on the holder of the two outer elements of the optical system.

50 The invention utilizes the fact that the optical behaviour of each of the elements determining the radiation beam and the wavelength of this beam are also dependent on the ambient temperature. The refractive index of these elements is dependent on the temperature, whilst these elements also exhibit a given coefficient of expansion. According to the invention the parameters of the optical elements are chosen to be such that the changes in the optical behaviour of the elements caused by temperature variations compensate the change in the optical behaviour of the optical system which is caused by the change in distance between the optical elements which change is due to expansion or shrinkage of the holder.

The optical elements may entirely consist of glass. These elements may alternatively be made of a synthetic material. Hitherto the use of synthetic material elements such as synthetic material lenses in

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optical systems has had the drawback that the refractive indices of the synthetic materials are temperature-dependent to a relatively large extent, whilst in addition the synthetic materials have a relatively large coefficient of expansion so that the optical behaviour of the elements varies to a relatively great extent with the temperature. This drawback is obviated when using the inventive idea according to which this variation is compensated by a suitable choice of the coefficient of expansion of the material of the holder accommodating the optical system.

It is noted that in the art of optics the problem of the influence of temperature variations on the behaviour of an optical system has been known for a long time and that it has been attempted in various manners to solve this problem. In the German Patent Application no. 2,830,341 laid open to public inspection it is established that the image field of a composite objective system shifts upon temperature changes due to the change in length of the objective holder. To solve this problem it is proposed to manufacture at least one of the fittings of the lens elements from a material which is different from the material of the fittings of the other elements. Furthermore United States Patent no. 4,162,120 states that temperature variations may result in expansion or shrinkage of glass lenses and cause changes in the refractive index of these lenses, and, in expansion or shrinkage of the lens fittings so that the focal length of the lens system varies. It is proposed as a solution to provide a special connection between the lens fittings and the holder which connection comprises alternately first and second elements which have high and low coefficients of expansion, respectively.

In none of the known optical systems the temperature coefficients of the elements are adapted to the coefficient of expansion of the holder accommodating these elements.

The Invention can be used advantageously in an optical device in the form of a radiation source unit supplying a collimated radiation beam and having a radiation source constituted by a diode laser whose wavelength is temperature-dependent and a collimator lens whose object focal plane must coincide with the radiating surface of the radiation source. This radiation source unit is characterized in that the collimator lens is a single lens and in that the equivalent coefficient of expansion giving the variation of the front focal length of the collimator lens as a function of the temperature is equal to the coefficient of expansion of the holder material which is present between the fixations on the holder of the radiation source and the collimator lens.

The front focal length is the length, measured along the optical axis, between the focus of the collimator lens and the refractive surface of this lens located on the side of this focus.

The invention can also be used advantageously in an optical device in the form of an optical detection unit for receiving a beam of radiation and comprising a lens for focussing the radiation beam and a radiation-sensitive detector to convert the radiation beam into an electrical signal. This detection unit is characterized in that the equivalent coefficient of expansion giving the variation of the focal length of the lens and the temperature dependency of the wavelength of the beam of radiation is equal to the coefficient of expansion of holder material which is present between the fixations on the holder of the radiation detector and the lens.

When using the a single lens the condition at which the variation in optical behaviour due to the variation of the lens compensates the variation caused by the change in length of the holder can be derived in a simple manner.

The simplest embodiment of the radiation source or detection unit comprising only a radiation source, respectively a detector, and a lens is characterized in that the lens is a planoconvex lens and in that the following condition is satisfied

$$\alpha_{eq} \cdot f_t = \alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_2} - \frac{f}{n_1} \right) \left(\frac{\partial n_1}{\partial \lambda} \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 L$$

in which

f_t is the front focal length,

α_{eq} is the equivalent optical coefficient of expansion,

f is the object focal length of the lens,

α_1 is the coefficient of expansion of the lens material,

D_1 is the axial thickness of the lens,

n_1 is the refractive index of the lens material,

α_2 is the coefficient of expansion of the holder material between the radiation source and the lens.

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L is the length of the holder between the radiation source and the lens, and $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

respect to the wavelength and temperature, respectively.

5 An embodiment of a single planoconvex collimator lens is described in United States Patent no. 4,592,627. The convex surface of this lens has an aspherical profile so that the lens is satisfactorily corrected for spherical aberrations.

Particularly in a radiation source unit which is intended for use in an optical write and/or read device, a diode laser is preferably used as a radiation source.

10 Instead of a planoconvex lens whose convex surface is aspherical, the lens may be alternatively a biconvex lens whose surfaces are aspherical or not aspherical. The embodiment of the optical device having such a lens is characterized in that the following condition is satisfied

$$15 \quad \left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \left(\frac{\partial n_1}{\partial \lambda} \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) \right\} +$$

$$20 \quad \left(\frac{f}{f_1} \frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \left(\frac{\partial n_1}{\partial \lambda} \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 \cdot L$$

in which

25 f is the optical focal length of the lens,

f_1 is the equivalent focal length of only the surface of the lens remote from the radiation source,

D_1 is the axial thickness of the lens,

n_1 is the refractive index of the lens material,

30 α_1 is the coefficient of expansion of the lens material,

R_2 is the radius of curvature of the surface of the lens facing the radiation source,

α_2 is the coefficient of expansion of the holder material between the radiation source and the lens and

35 L is the length of the holder between the radiation source and the lens, and

$\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

respect to wavelength and temperature, respectively.

By replacing R_2 and α_2 , the condition for a concave-convex lens whose concave surface has a radius of curvature R_1 is obtained.

When using a radiation source unit in a device for reading an optical record carrier having a radiation-reflecting information surface, a beam-separating element, for example a prism having a semitransparent interface is arranged between the radiation source and the collimator lens, as is shown in United States Patent n. 4,592,627. The purpose of this element is to separate the beam reflected by the information structure from the beam emitted by the radiation source and to direct the first-mentioned beam onto a radiation-sensitive detection system. By arranging such an element the optical path length between the radiation source and the collimator lens is changed and, since the material of this element has a coefficient of expansion and a temperature-dependent refractive index, temperature variations will influence the optical behaviour of this element and hence that of the radiation source unit.

According to the invention this effect may also be compensated by a suitable choice of the parameters of the other optical elements in the radiation source unit.

Such an optical device having a planoconvex lens is characterized in that the following condition is satisfied

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$$\begin{aligned}
 9 & \alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_2^2} - \frac{f}{n_1-1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) + D_3 \\
 10 & \left\{ \frac{n_3-1}{n_3} \alpha_3 + \frac{1}{n_3^2} \left(\frac{\partial n_3}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_3}{\partial T} \right) \right\} = \alpha_2 \cdot L.
 \end{aligned}$$

in which D_3 , n_3 , and α_3 are the axial thickness of the beam-separating element, the refractive index of the element material and the coefficient of expansion of this material, respectively. The other quantities of this equation have been defined hereinbefore.

15 An optical device having a beam-separating prism and a biconvex lens is characterized in that the following condition is satisfied

$$\begin{aligned}
 20 & \left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) \right. \\
 25 & \left. \left(\frac{f}{f_1} \frac{D_1}{n_1^2} - \frac{f}{n_1-1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) + D_3 \right\} \\
 30 & \left(\frac{\partial n_3}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_3}{\partial T} \right) = \alpha_2 \cdot L.
 \end{aligned}$$

35 The invention also relates to a device for scanning an information plane in an optical record carrier, which device comprises a radiation source supplying a scanning beam, an objective system for focussing the scanning beam to a scanning spot in the information plane and a detection unit for converting the beam from the record carrier into an electrical signal. The sensitivity to temperature variations of such a device is limited if this device is characterized in that the radiation source unit and/or the detection unit are in the form of one of the above-mentioned embodiments according to the invention.

40 The invention will now be described in greater detail by way of example with reference to the accompanying drawings in which

Figure 1 shows a known device for both writing and reading an optical record carrier.

Figure 2 shows a radiation source unit according to the invention for use in this device.

Figure 3 shows a planoconvex collimator lens for use in the radiation source unit,

Figure 4 shows a biconvex collimator lens,

45 Figure 5 shows a device for reading an optical record carrier having a read unit which is provided with a beam-separating prism, and

Figure 6 shows a telecentric lens system.

50 Figure 1 shows a perspective view a part of a round disc-shaped record carrier 1. The information plane 2 of this carrier in which a user can write information and read it afterwards is located on the upper side of the record carrier so that writing and reading is effected through the carrier substrate 3 by means of a write spot WS and a read spot RS, respectively. A previously provided servo-track 4 of which only a small part is shown in Figure 1 is present in the information plane 2. By rotating, in the direction of the arrow 7, the record carrier about a shaft 6 inserted through a central opening 5 in the carrier the spots can scan a revolution of the servo-track 4. The entire spiral-shaped servo-track is scanned by a defined movement of the two spots in the radial direction.

55 The write and read device has two radiation source units 10 and 11 supplying a write beam WB and a read beam RB, respectively. These beams are directed towards an objective system 15 by means of a reflector 14 which is adjustable, for example in the tangential and radial directions, and the objective system

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focuses the beam WB to a write spot WS and the beam RB to a read spot RS in the information surface.

The beams WB and RB emitted by the radiation source units 10 and 11 are linearly and mutually perpendicularly polarized. A beam-splitter 13, for example a partially transparent prism is arranged in the path of the beam RB, which prism reflects this beam to a polarisation-sensitive beam splitter 12, for example in the form of a prism. This prism reflects both the beam RB from the radiation source unit and the beam RB' reflected by the information plane. The write beam WB is passed by the beam splitter 12 and traverses a highly selective $\lambda/4$ plate 18 twice on its path to and from the information plane. λ is the wavelength of the beam WB. The plate 18 rotates the direction of polarisation of only the write beam through 90° so that the reflected beam WB is reflected by the beam splitter 12. The highly selective plate 18 does not have any influence on the direction of polarisation of the read beam RB.

The beams WB' and RB' which are reflected by the beam splitter 12 and which have the same direction of polarisation are passed by the prism 13 to their associated detectors 22 and 23. The beams WB' and RB' may be separated from each other by, for example the combination of a highly selective $\lambda/2$ -plate 18, which rotates the direction of polarisation of one of the beams through 90°, and a polarisation-sensitive beam separator 19 which substantially passes one of the beams, for example WB' and substantially reflects the other beam to the detectors 22 and 23, respectively. Wavelength-selective filters 20 and 21 may be arranged in front of the detectors, which filters prevent radiation of the write beam and the beam from reaching the detector for the read beam and the write beam, respectively. The lens 17 focuses the parallel beams WB' and RB' on the detectors 22 and 23.

For further details about writing and reading with the device according to Figure 1 and about the servo-systems used for tracking and focusing reference is made to United States Patent no. 4,546,463 in which other embodiments of the write-read device based on the same principle are described.

For a satisfactory operation of the device it is required for the beams entering the objective system to have a constant cross-section, in other words the radiation source units should supply beams which are constantly collimated, independent of temperature variations.

As is shown in Figure 2 each radiation source unit 10 and 11 comprises a holder 30, for example of aluminium or stainless steel. This holder has an abutment 31. A radiation source in the form of a diode laser 33 has a flange 34 whose top face engages the abutment 31 and whose side face engages the inner wall of the holder. The diode laser is fixed in the holder by means of the bent edges 32. Furthermore the holder 30 comprises a collimator lens 37 which is arranged between the bent edges 40 and is fixed against the inner wall of the holder, for example by means of an adhesive. The holder may be closed by means of a transparent plate 41. The radiation source unit may further have a cylindrical lens at the area of the plate 41 or between this plate and the radiation source for correction of possible astigmatism of the beam.

The collimator lens is for example a planoconvex lens whose plane surface 38 faces the diode laser. It must be ensured that the distance between the surface 38 and the diode laser is such that the radiating surface 36 of the diode laser is located in the focal plane of the collimator lens. However, under the influence of temperature variations the holder may expand or shrink so that the distance between the radiating surface 36 and the surface 38 of the collimator lens changes, which results in the surface 36 no longer coinciding with the focal plane of the collimator lens and in the beam WB or RB emanating from this lens no longer being collimated. According to the invention the reflective index, the coefficient of expansion and the other lens parameters are chosen to be such that the length variation of the holder is compensated for.

The condition under which this is effected will now be described with reference to Figure 3. In this figure F. is the object focus in which focus the radiating surface of the laser must be located. f is the focal length, or the distance between the focus F. and the principal plane H of the lens. f_1 is the so-called front focal length, that is to say the distance, measured along the optical axis O⁰, between the surface 38 of the lens and the focus F.. L_1 is the distance between the surface 38 and the principle plane H and D. is the axial thickness of the collimator lens. R. is the radius of the curvature of the convex surface 39 of the lens. It is assumed that the lens is secured in the holder at the position of the surface 38 and that the radiation source is secured in the holder at the position of the radiating surface of this source. The expansion $\frac{dL}{dT} = \alpha_1 L$ of the holder portion having a length L between the said areas of fixation must then be equal to the change

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$$\frac{df_1}{dT} \cdot \alpha_2$$

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is the coefficient of expansion of the holder material.

As is apparent from Figure 3

$$f_t = f - L_H \quad (1)$$

The focal length f_t of a planoconvex lens is given by

5

$$f = \frac{R_1}{n_1 - 1} \quad (2)$$

10 in which n_1 is the refractive index of the lens material. For L_H it holds that
 $L_H =$

15

$$\frac{D_1}{n_1}$$

Therefore it holds that

20

$$f_t = \frac{R_1}{n_1 - 1} - \frac{D_1}{n_1} \quad (3)$$

25 In the case of temperature variations both the geometry of the lens, and hence the quantities R_1 and D_1 , and the refractive index n_1 changes so that

30

$$\frac{df_t}{dT} = \frac{1}{n_1 - 1} \cdot \frac{dR_1}{dT} + \frac{R_1}{(n_1 - 1)^2} \cdot \frac{dn_1}{dT} - \frac{1}{n_1} \cdot \frac{dD_1}{dT} +$$

$$\frac{D_1}{n_1^2} \cdot \frac{dn_1}{dT}$$

35

(4)

By filling in

40

$$\frac{1}{R_1} - \frac{dR_1}{dT} = \alpha_1 = \frac{1}{D_1} - \frac{dD_1}{dT}$$

45

with α_1 being the coefficient of expansion of the lens material, and

50

$$\frac{R_1}{n_1 - 1} = f$$

equation (4) changes into

$$55 \quad \frac{df_t}{dT} = \alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \frac{dn_1}{dT} = \alpha_{eq} \cdot f_t \quad (5)$$

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in which α_{eq} can be indicated as an equivalent coefficient of expansion, or in other words the change of the focal length per degree of temperature changes due to changes within the optical system. According to the invention it is ensured that

$\alpha_{eq} \cdot f_1 = \alpha_1 \cdot L$ so that, f_1 and L are equal $\alpha_{eq} = \alpha_1$.

9 The radiation source which is used in the radiation source unit is preferably a diode laser, for example an AlGaAs laser. For such a laser the wavelength λ of the emitted radiation can vary with the temperature. A great advantage of the present invention is that this variation can also be compensated for by taking this variation into account when choosing the parameters in equation (5).

10 Since the refractive index n of the lens material depends on the wavelength of the radiation passing through the lens,

$$\frac{dn_1}{d\lambda}$$

15 In equation (5) must be replaced by

$$\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T}$$

20

In which the symbols $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ denote the

25 partial derivatives with respect to wavelength and temperature, respectively. According to the invention, for a radiation source unit having a radiation source whose wavelength depends on the temperature it holds that

$$30 \quad \alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 L.$$

35

(6)

40 Instead of a planoconvex lens, a lens having two curved refractive surfaces may be used alternatively as a collimator lens, for example a biconvex lens.

Figure 4 shows a biconvex lens. As is known from the Handbooks on Optics it holds for the focal length f of a biconvex lens that:

$$45 \quad f = \frac{R_1 R_2}{n_1 - 1} \cdot \frac{1}{\frac{R_1 + R_2 - D_1}{R_1} - \frac{n_1 - 1}{n_1}}$$

50

(7)

and the front focal length is given by:

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$$f_t = f \left(1 - \frac{n_1 - 1}{n_1} \frac{D_1}{R_1} \right) = f \left(1 - \frac{D_1}{n_1} \frac{1}{f_1} \right) \quad (8)$$

in which

$$f_1 = \frac{R_1}{n_1 - 1}$$

so that

$$\frac{df_t}{dT} = \left(1 - \frac{D_1}{n_1} \frac{1}{f_1} \right) \frac{df}{dT} + f \frac{d}{dT} \left(1 - \frac{n_1 - 1}{n_1} \frac{D_1}{R_1} \right) \quad (9)$$

since D_1 and R_1 relate to the same material:

$$\frac{d}{dT} \frac{D_1}{R_1} = 0$$

so that for the second term on the right-hand side in (9) it holds that:

$$f \frac{d}{dT} \left(1 - \frac{n_1 - 1}{n_1} \cdot \frac{D_1}{R_1} \right) = f \frac{D_1}{R_1} \cdot \frac{d}{dT} \left(\frac{n_1 - 1}{n_1} \right)$$

Consequently it holds that

$$f \frac{d}{dT} \left(1 - \frac{n_1 - 1}{n_1} \frac{D_1}{R_1} \right) = -f \frac{D_1}{R_1} \frac{1}{n_1^2} \frac{dn_1}{dT} = -\frac{f}{n_1^2} \cdot D_1 \cdot \frac{1}{n_1 - 1} \cdot \frac{dn_1}{dT}$$

(10)

For the lens according to Figure 4 it also holds that

$$f = f_1 \cdot \frac{\frac{R_2}{n_1 - 1}}{R_1 + R_2 - D_1 \cdot \frac{1}{n_1}} \quad (11)$$

so that

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$$5 \quad \frac{df}{dT} = \frac{R_2}{R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1}} \cdot \frac{df_1}{dT} + f_1 \cdot \frac{d}{dT} \frac{R_2}{R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1}}$$

Since R_1 , R_2 and D_1 relate to the same material it holds that:

$$10 \quad f_1 \cdot \frac{d}{dT} \cdot \frac{R_2}{R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1}} = - \frac{f_1 R_2}{(R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1})^2} \cdot D_1 \cdot \frac{d}{dT} \left(\frac{n_1 - 1}{n_1} \right)$$

15

so that:

$$20 \quad 25 \quad \frac{df}{dT} = \frac{f}{f_1} \cdot \frac{df_1}{dT} - \frac{f_1 R_2}{(R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1})^2} \cdot D_1 \cdot \frac{d}{dT} \left(\frac{n_1 - 1}{n_1} \right)$$

30 and hence:

$$25 \quad 30 \quad \frac{df}{dT} = \frac{f}{f_1} \cdot \frac{df_1}{dT} + \frac{f D_1}{n_1^2} \cdot \frac{1}{R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1}} \cdot \frac{dn_1}{dT}$$

(12)

40 In this expression f , corresponds to f in the expression (2) for the planoconvex lens from which it can be derived that:

$$45 \quad \frac{1}{f_1} \cdot \frac{df_1}{dT} = \alpha_1 - \frac{1}{n_1 - 1} \cdot \frac{dn_1}{dT}$$

(13)

so that (12) can be written as:

$$50 \quad 55 \quad \frac{df}{dT} = f \left(\alpha_1 - \frac{1}{n_1 - 1} \cdot \frac{dn_1}{dT} \right) + \frac{f D_1}{R_1 + R_2 - D_1 \frac{n_1 - 1}{n_1}} \cdot \frac{1}{n_1^2} \cdot \frac{dn_1}{dT}$$

(14)

and hence:

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$$s \quad \frac{1}{f} \frac{df}{dT} = \alpha_1 + \left\{ \frac{fD_1}{f_1 \cdot n_1^2 \cdot R_2} - \frac{1}{n_1 - 1} \right\} - \frac{dn_1}{dT} \quad (15)$$

10 Filling in (10) and (15) and (9) results in:

$$15 \quad \frac{df}{dT} = (f - \frac{D_1}{n_1} \frac{f}{f_1}) \left\{ \alpha + \left(\frac{f \cdot D_1}{f_1 n_1^2 R_2} - \frac{1}{n_1 - 1} \right) \frac{dn_1}{dT} \right\} - \frac{f D_1}{f_1 n_1^2} \cdot \frac{1}{n_1 - 1} + \frac{dn_1}{dT}$$

$$20 \quad (16)$$

25 whose right-hand term can be arranged as:

$$30 \quad \frac{df}{dT} = (f - \frac{f}{f_1} \frac{D_1}{n_1}) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} - \frac{dn_1}{dT} \right\} + \left(\frac{f}{f_1} - \frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \frac{dn_1}{dT} = \alpha_2 L.$$

$$35 \quad (17)$$

40 If a biconvex collimator lens in the radiation source unit is combined with a diode laser whose wavelength is temperature-dependent,

$$\frac{dn_1}{dT}$$

45 in expression (17) must be replaced by

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$\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T}$ so that:

$$9 \quad \left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \left(\frac{\partial n_1}{\partial \lambda} \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) \right\} +$$

$$10 \quad \left(\frac{f}{f_1} \frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \left(\frac{\partial n_1}{\partial \lambda} \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 \cdot L$$

11 (18)

If in (18) R_2 is provided with a minus-sign, the condition for temperature compensation is obtained for a 20 radiation source unit having a concave-convex collimator lens whose concave surface has a radius of curvature R_2 .

25 Figure 5 shows diagrammatically a radiation source unit 50 which in combination with an objective system 51 and a built-in radiation-sensitive detection system 42 constitutes a read device which is particularly suitable for reading optical record carriers. For the operation of this device reference is made to the United States Patent no. 4,592,827 in which the device has been described in detail. In connection with the present invention it is only important that a beam-separating element, for example in the form of a partially transparent prism 53 is arranged between the diode laser 33 and the collimator lens 37. This prism passes a part of the beam R_B emitted by the diode laser to the record carrier 1 and reflects a part of the beam reflected by the information plane 2 to the radiation-sensitive detection system 52.

30 By arranging the prism in the radiation path the optical path length changes by

$$D_3 \cdot \frac{n_3 - 1}{n_3}$$

35 in which D_3 is the thickness of the prism, measured along the optical axis OD' and n_3 is the refractive index of the prism material. For the optical path length S between the radiating surface of the diode laser and the collimator lens 37 it now holds that:

$$40 \quad S = f_t + D_3 \cdot \frac{n_3 - 1}{n_3}$$

45 (19)

and for the change caused by the temperature variations it holds that:

$$60 \quad \frac{dS}{dT} = \frac{df_t}{dT} + \frac{n_3 - 1}{n_3} \frac{dD_3}{dT} + D_3 \cdot \frac{d}{dT} \left(\frac{n_3 - 1}{n_3} \right).$$

55 hence

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$$\frac{ds}{dt} = \frac{df_t}{dt} + \frac{n_2 - 1}{n_3} \alpha_3 \cdot D_3 + \frac{D_3}{n_2} \frac{dn_3}{dt} \quad (20)$$

If, as shown in Figure 5, the collimator lens is a planoconvex lens, the expression (5) can be filled in for

$$\frac{df_t}{dt}$$

and

$$\begin{aligned} \frac{ds}{dt} &= \alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \frac{dn_1}{dt} + \frac{D_3}{n_3} \left\{ (n_3 - 1) \alpha_3 + \frac{1}{n_3} \frac{dn_3}{dt} \right\} \\ &= \alpha_2 L. \end{aligned} \quad (21)$$

If the collimator lens is a biconvex lens

$$\frac{df_t}{dt}$$

must be replaced by the expression (17) so that:

$$\begin{aligned} \frac{ds}{dt} &= \left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \cdot \frac{n_1}{\alpha_1 T} \right\} + \left(\frac{f}{f_1} \frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \cdot \\ &\quad \frac{dn_1}{dt} + \frac{D_3}{n_3} \left\{ (n_3 - 1) \alpha_3 + \frac{1}{n_3} \frac{dn_3}{dt} \right\} = \alpha_2 L. \end{aligned} \quad (22)$$

If the radiation source is a diode laser with a temperature-dependent wavelength, $\frac{dn}{dT}$ in the expressions 21 and 22 must be replaced by

$$\frac{\partial n_s}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_s}{\partial T}$$

If the collimator lens is a planoconvex lens, its convex surface preferably has an aspherical profile in order to correct for spherical aberrations. As described in the United States Patent no. 4,592,827 and as shown in Figure 5, the aspherical surface may be in the form of an aspherical outer profile 57 of a thin layer of transparent synthetic material 58 which is provided on the convex surface 55 of the lens 37. In the aforementioned expressions for the equivalent coefficient of expansion there are no quantities which relate to this synthetic material layer because, due to the small thickness of the layer, the temperature effects in the layer hardly have any influence on the focal length of the overall optical system within the holder.

Certain types of diode lasers emit an astigmatic beam, i.e. a beam which, viewed in two mutually perpendicular planes, has two axially shifted points of convergence. When using this type of laser in an

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optical radiation source unit, a cylindrical lens is generally used to render the beam stigmatic. This cylindrical lens may be integrated with the collimator lens by superposing the required cylindrical shape on the surface of the collimator lens facing the diode laser. In that case the above given expressions for the equivalent coefficient of expansion remain valid because the radius of curvature of the said cylindrical lens is of the order of a hundred times that of the convex surface of the collimator lens so that the position of the focus of the optical system within the holder is substantially uninfluenced by the presence of the cylindrical lens and by variations in the behaviour of this lens.

It has been assumed in the foregoing that the radiation source in the holder is secured at the position of the radiating surface and that the collimator lens is secured at the position of the point of intersection of the surface 38 and the optical axis. If the fixations are located elsewhere, the coefficient of expansion of the portions of the holder between the points of fixation and the axial positions of the radiating surface of the radiation source and the surface of the collimator lens facing the radiation source must be taken into account, as is known from, for example German Patent Application No. 2,830,341. The influence of the changes of these portions can be calculated and the above given conditions for the temperature compensation can then be corrected.

A radiation source unit supplying a collimated beam can also be used in a so-called target-seeking device with which a target can be traced and/or followed by means of a beam emitted by the radiation source unit and received by a radiation-sensitive detector. The temperature compensation according to the invention can also be used in this device.

The invention has been described on the hand of a radiation source unit for use in an optical recording and/or reading apparatus. Such apparatus comprises also a detection unit which, as shown in the cited US Patent 4,548,463 may be of similar construction as the radiation source unit. This detection unit comprises in principle a radiation sensitive detector and a lens for focussing an incident radiation beam to a spot on the detector and can be represented by a figure like Figure 2 wherein diodelaser 33 is replaced by a detector like a photodiode. The detection unit may suffer from the same temperature effects as the radiation source unit. The present invention can also be used to ensure that the spot formed on the detector is not influenced by temperature effects.

The invention is not limited to a radiation source or -detection - unit but may be generally applied in optical systems whose optical behaviour should not be influenced by a change of the holder accommodating this system. A system which must have a constant factor of magnification such as a telecentric system shown diagrammatically in Figure 6 may be mentioned as an example.

A telecentric lens system comprises a number of, for example two lenses, L_1 and L_2 in Figure 6, with given powers and mutual distances. If the centre of the so-called aperture stop AA' of this system is located in the focus F_1 of the lens L_1 , the exit pupil of the system, i.e. the image of the aperture stop formed by the lens L_2 is located at infinity and the system is telecentric on the image side. This means that the chief ray h of each beam b traversing the system is perpendicularly incident on the image plane IP . If the aperture stop is in the focus F_2 of the lens L_2 , the entrance pupil is located at infinity and the system is telecentric on the object side. OP' is the object plane which is conjugated to the image plane IP . In a double telecentric system as is shown in Figure 6, F_1 and F_2 both coincide with the centre of the aperture stop. According to the invention the variation of the distance between the lenses which is caused by a temperature-dependent variation in length of the holder H , can be compensated by adapting the coefficients of expansion and the refractive indices of the lenses to the coefficient of expansion of the holder. Analogously as described above for a radiation source unit, the condition at which the temperature compensation occurs can be derived for a telecentric system.

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Claims

1. An optical device comprising a holder accommodating a system of optical elements, inter alia a lens system, which elements are secured to the inner wall of the holder, characterized in that the equivalent coefficient of expansion of the optical system giving the change in the optical behaviour of this system as a function of the temperature and being determined by:
 - the coefficient of expansion of the materials of the optical elements,
 - the refractive indices of these materials and their variations with temperature,
 - the dimensions of the optical elements, and
 - the temperature-dependency of the wavelength of the optical beam passing through the device is equal to the coefficient of expansion of the holder material which is located between the fixations on the holder of the two outer elements of the optical systems.

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2. An optical device as claimed in Claim 1 in the form of an optical radiation source unit supplying a collimated radiation beam and having a radiation source constituted by a diode laser whose wavelength is temperature dependent and a collimator lens whose object focal plane must coincide with the radiating surface of the radiation source, characterized in that the collimator lens is a single lens and in that the equivalent coefficient of expansion giving the variation of the front focal length of the collimator lens as a function of the temperature is equal to the coefficient of expansion of the holder material which is present between the fixations on the holder of the diodelaser source and the collimator lens.

3. An optical device as claimed in Claim 1, in the form of an optical detection unit for receiving a beam of radiation comprising a lens for focussing the radiation beam and a radiation sensitive detector to convert the radiation beam into an electrical signal, characterizing in that the equivalent coefficient of the expansion giving the variation of the focal length of the lens and the temperature dependency of the radiation beam passing through the device is equal to the coefficient of expansion of the holder material which is present between the fixations on the holder of the radiation detector and the lens.

4. An optical device as claimed in Claim 2 or 3, characterized in that the lens is a planoconvex lens and in that the following condition is satisfied:

$$20 \quad \alpha_1 \left(f \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_2} - \frac{f}{n_1-1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 L.$$

in which:

α_{eq} is the equivalent optical coefficient of expansion,
 25 f_1 is the front focal length,
 f is the object focal length of the lens
 α_1 is the coefficient of linear expansion of the lens material,
 D_1 is the axial thickness of the lens,
 n_1 is the refractive index of the lens material,
 30 α_2 is the coefficient of linear expansion of the holder material between the radiation source and the lens and
 L is the length of the holder between the radiation source and the lens and
 $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

35 respect to wavelength and temperature, respectively.

5. An optical device as claimed in Claim 2 or 3, whose lens is a biconvex lens, characterized in that the following condition is satisfied:

$$40 \quad \left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) \right\} + \\ 45 \quad \left(\frac{f}{f_1} \frac{D_1}{n_2} - \frac{f}{n_1-1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) = \alpha_2 L.$$

in which:

f is the object focal length of the lens,
 50 α_1 is the coefficient of linear expansion of the lens material,
 f_1 is the equivalent focal length of only the surface of the lens remote from the radiation source,
 D_1 is the axial thickness of the lens,
 n_1 is the refractive index of the lens material,
 R_2 is the radius of curvature of the surface of the lens facing radiation source,
 55 α_2 is the coefficient of linear expansion of the holder material between the radiation source and the lens,
 L is the length of the holder between the radiation source and the lens and
 $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

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respect to wavelength and temperature, respectively.

8. An optical device as claimed in Claim 2 or 3, in which a beam-separating element is arranged between the lens and the radiation source or detector, characterized in that the following condition is satisfied:

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$$\alpha_1 \left(f - \frac{D_1}{n_1} \right) + \left(\frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) + D_3$$

10

$$\left\{ \frac{n_3 - 1}{n_3} \alpha_3 + \frac{1}{n_3^2} \left(\frac{\partial n_3}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_3}{\partial T} \right) \right\} = \alpha_2 \cdot L.$$

15

in which:

- a. is the coefficient of linear expansion of the lens material,
- b. is the object focal length of the lens,
- c. is the axial thickness of the lens,
- d. is the refractive index of the lens material,
- e. is the axial thickness of the beam-separating element,
- f. is the refractive index of the material of this element,
- g. is the coefficient of linear expansion of the element material,
- h. is the length of the holder between the radiation source and the lens,
- i. is the coefficient of linear expansion of the holder material between the radiation source and the lens,
- and
- $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

respect to wavelength and temperature, respectively.

9. An optical device as claimed in Claim 2 or 3, in which a beam-separating element is arranged between the radiation source or detector and the lens, characterized in that the lens is a biconvex lens and in that the following condition is satisfied:

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$$\left(f - \frac{f}{f_1} \frac{D_1}{n_1} \right) \left\{ \alpha_1 + \frac{f}{f_1} \frac{D_1}{n_1^2 R_2} \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) \right\} +$$

40

$$\left(\frac{f}{f_1} \frac{D_1}{n_1^2} - \frac{f}{n_1 - 1} \right) \left(\frac{\partial n_1}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_1}{\partial T} \right) + D_3 \left\{ \frac{n_3 - 1}{n_3} \alpha_3 + \frac{1}{n_3^2} \right.$$

45

$$\left. \left(\frac{\partial n_3}{\partial \lambda} \cdot \frac{\partial \lambda}{\partial T} + \frac{\partial n_3}{\partial T} \right) \right\} = \alpha_2 \cdot L.$$

50 In which:

- f. is the object focal length of the lens,
- g. is the equivalent focal length of only the surface of the lens remote from the radiation source,
- h. is the axial thickness of the lens,
- i. is the refractive index of the lens material,
- j. is the coefficient of linear expansion of the lens material,
- k. is the radius of curvature of the surface of the lens facing the radiation source,
- l. is the axial thickness of the beam-separating element,
- m. is the refractive index of the material of this element.

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α_1 is the coefficient of linear expansion of the element material,
 α_2 is the coefficient of the linear expansion of the holder material between the radiation source and the lens and

5 L is the length of the holder between the radiation source and the lens, and
 $\frac{\partial}{\partial \lambda}$ and $\frac{\partial}{\partial T}$ are the partial derivatives with

respect to wavelength and temperature, respectively.

8. A device for scanning an information plane in an optical record carrier, which device comprises a radiation source supplying a scanning beam, an objective system for focussing the scanning beam to a scanning spot in the information plane, and a detection-unit for converting the beam from the record carrier into an electrical signal, characterized in that the radiation source unit and/or the detection unit are in the form of an optical device as claimed in any one of Claims 2-7.

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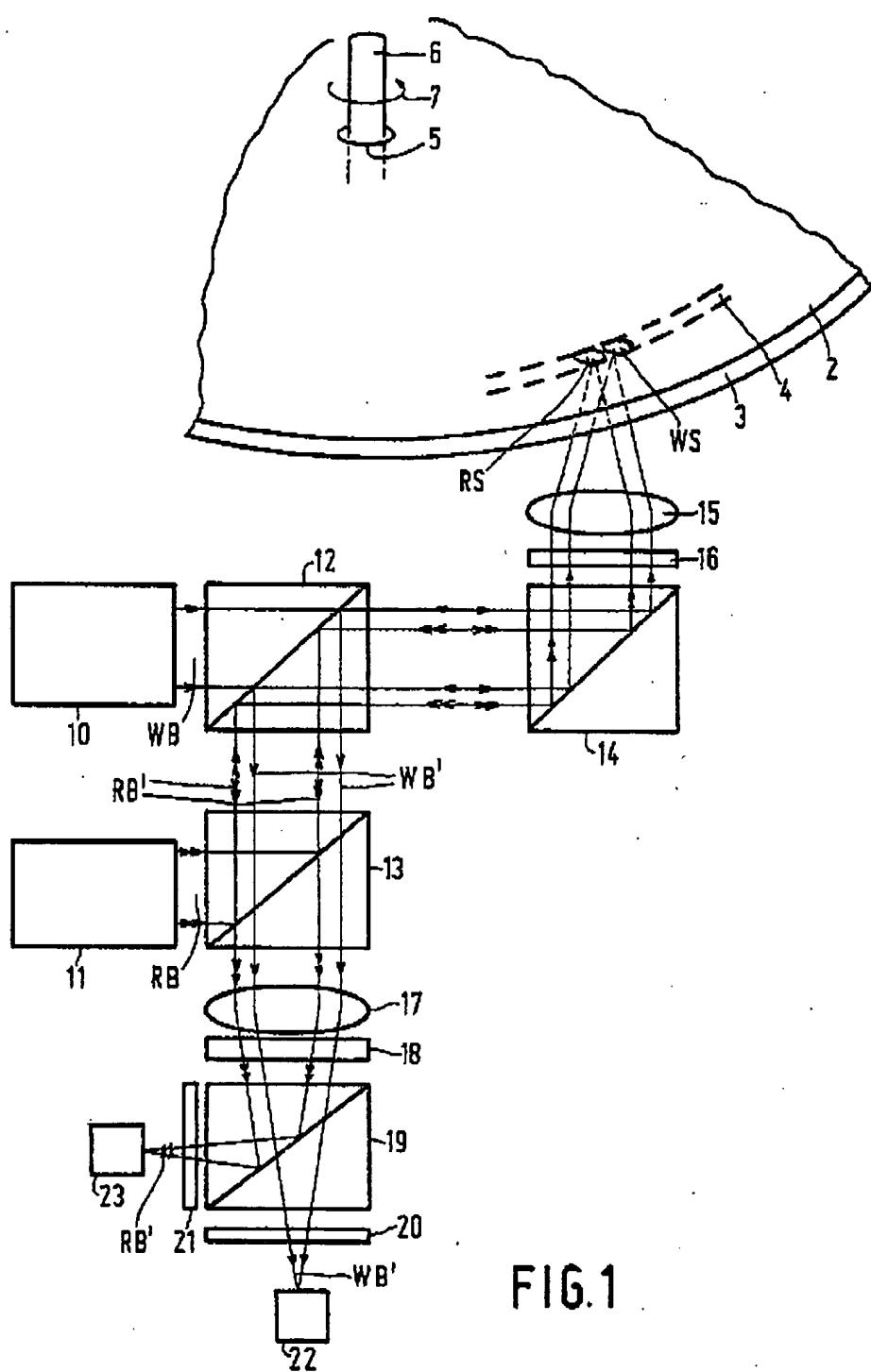


FIG.1

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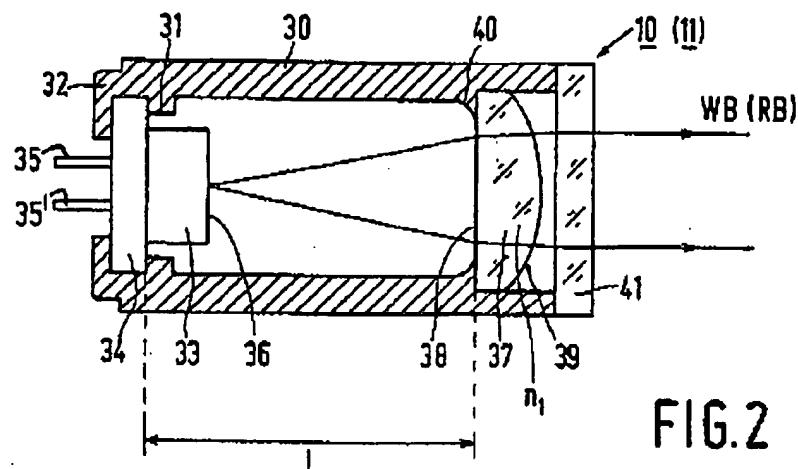


FIG.2

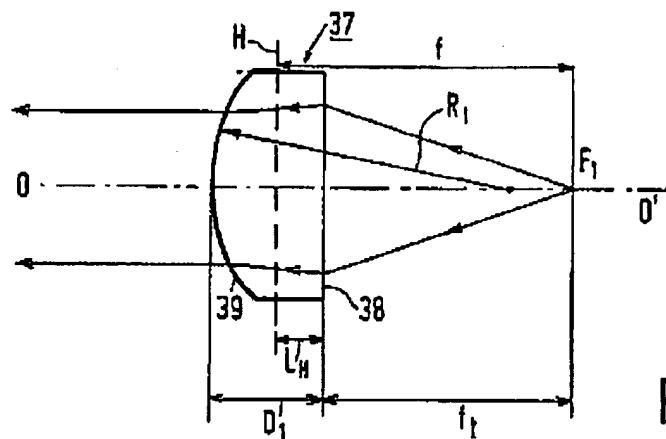


FIG.3

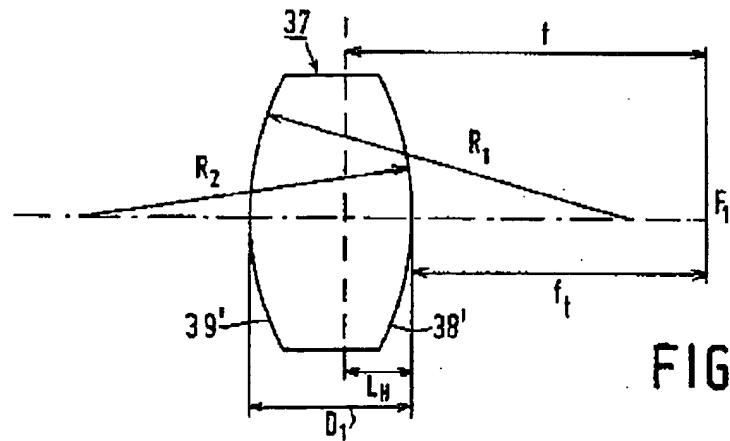


FIG.4

2-III-PHN 12042

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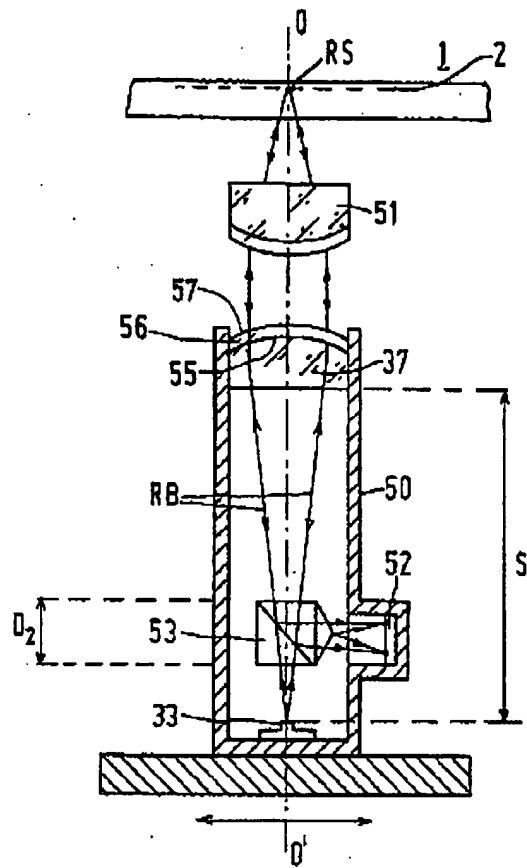


FIG.5

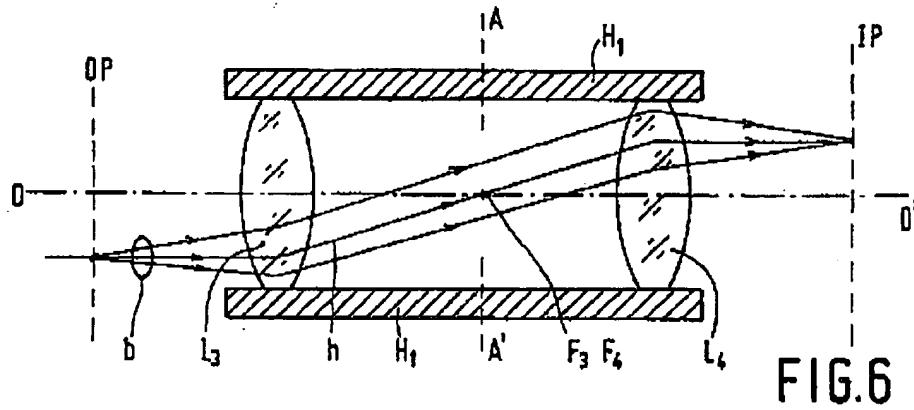


FIG.6

3-III-PHN 12042



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Application Number

EP 88 20 0293

DOCUMENTS CONSIDERED TO BE RELEVANT			CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)		
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 4)		
X	PATENT ABSTRACTS OF JAPAN, vol. 10, no. 124 (P-454)[2181], 9th May 1986; & JP-A-60 250 316 (NIHON KOGAKU KOGYO K.K.) 11-12-1985 ---	1-3	G 02 B 7/00 G 11 B 7/12 H 01 S 3/02 H 01 S 3/13		
X	PATENT ABSTRACTS OF JAPAN, vol. 10, no. 369 (P-525)[2426], 10th December 1986; & JP-A-61 162 014 (RICOH CO LTD) 22-07-1986 ---	1-3			
A	EP-A-0 146 762 (TOSHIBA K.K.) * Page 4, line 14 - page 20, line 33; figures 1-8 *	1-3,5			
D,A	DE-A-2 830 341 (OLYMPUS OPTICAL CO.) * Whole document *	1			
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D,A	GB-A-2 097 150 (PHILIPS' GLOEILAMPENFABRIEKEN) * Whole document *	1,8	TECHNICAL FIELDS SEARCHED (Int. Cl. 4) G 02 B 7/00 G 02 B 27/00 G 11 B 7/00 H 01 S 3/00		
The present search report has been drawn up for all claims					
Place of search	Date of completion of the search	Examiner			
THE HAGUE	07-04-1988	SARNEEL A.P.T.			
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